

Tunable high Q perovskite dielectrics in the BaO–NiO–Ta₂O₅ system

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Introduction

Oxide perovskites with the general formula $A(B_{1/3}^I B_{2/3}^{II})O_3$ ($A = \text{Ba, Sr}$; $B^I = \text{Mg, Zn, Ni, Co, etc.}$; $B^{II} = \text{Ta, Nb}$) have been investigated for over two decades for applications as dielectric resonators in wireless communication systems. The key materials requirements include a high dielectric constant (ϵ), low dielectric loss or high quality factor (Q) in the GHz range, and a zero temperature coefficient of resonant frequency (τ_f). Recent investigations of the effect of Zn volatilization on the properties of one of the most studied high Q systems, $\text{Ba}(\text{Zn}_{1/3}\text{Ta}_{2/3})\text{O}_3$ (BZT), revealed a resultant Zn-deficient impurity phase, $\text{Ba}_8\text{ZnTa}_6\text{O}_{24}$ also exhibits a good microwave response ($\epsilon = 30.5$, $Q \cdot f = 62,000$, $\tau_f = +36 \text{ ppm}/^\circ\text{C}$) [1–3]. This phase, which has a closely related hexagonal perovskite structure (Fig. 1), can also be sintered at temperatures significantly lower than its cubic perovskite counterpart.

While the positive value of τ_f precludes the use of $\text{Ba}_8\text{ZnTa}_6\text{O}_{24}$ for commercial resonator applications, it is possible additives could tune τ_f to a zero value. Isotypic hexagonal perovskites containing other transition metal cations instead of Zn (e.g., Ni, Co) can be stabilized and have high Q values, however, they also have positive values of τ_f [4, 5]. Although the positive τ_f of $\text{Ba}_8\text{NiTa}_6\text{O}_{24}$ and $\text{Ba}_8\text{CoTa}_6\text{O}_{24}$ precludes direct tuning of the hexagonal systems, their cubic perovskite counterparts ($\text{Ba}(\text{Ni}_{1/3}\text{Ta}_{2/3})\text{O}_3$

and $\text{Ba}(\text{Co}_{1/3}\text{Ta}_{2/3})\text{O}_3$) have negative τ_f 's. This offers an opportunity for tuning their temperature coefficient via the formation of two-phase hexagonal/cubic perovskite “composites”. With that goal in mind, this study describes an investigation of the phase compatibility and dielectric properties of the nickel-based $(1-x)\text{Ba}(\text{Ni}_{1/3}\text{Ta}_{2/3})\text{O}_3-(x)$ “ $\text{Ba}(\text{Ni}_{1/8}\text{Ta}_{3/4})\text{O}_3$ ” ($=\text{Ba}_8\text{NiTa}_6\text{O}_{24}$) system.

Experimental

Samples of $\text{Ba}_8\text{NiTa}_6\text{O}_{24}$, $\text{Ba}_8\text{CoTa}_6\text{O}_{24}$, and compositions within the $(1-x)\text{Ba}(\text{Ni}_{1/3}\text{Ta}_{2/3})\text{O}_3-(x)\text{Ba}(\text{Ni}_{1/8}\text{Ta}_{3/4})\text{O}_3$ system were prepared by standard solid state techniques from dried powders of BaCO_3 (99.9%, Cerac, Inc., Milwaukee, WI), NiO (99.99%, Aldrich, Milwaukee, WI), Co_3O_4 (>99%, J. T. Baker, Phillipsburg, N.J.), and Ta_2O_5 (99.99%, Cerac). After weighing and mixing, the samples were ball-milled with ethanol. The dried powders were calcined at 1000 °C for about 13 h to remove CO_2 and subsequently ball-milled with ethanol. The final reactions were completed on uniaxially pressed pellets of the calcined powders heated to 1350–1475 °C for about 24–40 h, depending on the composition. The pellets were crushed, ground and isostatically pressed at 565 MPa and sintered at 1400–1500 °C; all of the ceramics were >95% of their theoretical density. For some samples a two stage sintering technique was used to avoid problems associated with exaggerated grain growth of the hexagonal perovskite phase [6].

Powder X-ray diffraction patterns were collected (Model DMAX-B diffractometer, Rigaku Co., Tokyo, Japan), using $\text{Cu K}\alpha$ radiation generated at 45 kV and 30 mA. Polished and thermally etched sintered pellets were

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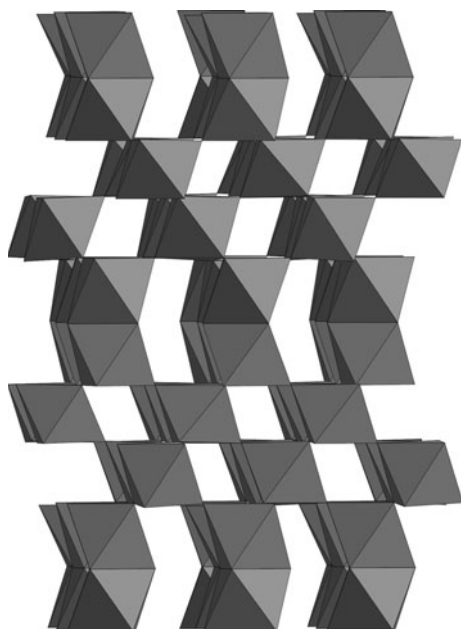


Fig. 1 8-layer hexagonal structure of $\text{Ba}_8\text{CoTa}_6\text{O}_{24}$ and $\text{Ba}_8\text{NiTa}_6\text{O}_{24}$ projected along $[1\bar{1}0]$ to highlight the corner and face shared octahedra, Ba atoms are omitted for clarity

examined using a scanning electron microscope (Model 6300FV cold field-emission, JEOL, Tokyo, Japan).

The relative permittivity and dielectric loss tangent were measured in the 100 Hz to 1 MHz frequency range from -100 to 100 °C using the parallel plate method (Model HP 4284A precision LCR meter, Hewlett-Packard, Palo Alto, CA). The microwave dielectric properties were measured using the cavity method with a network analyzer (Agilent 8720ES, S-Parameter network analyzer). The $\text{TE}_{01\delta}$ mode was identified and the permittivity and unloaded Q values were calculated at resonant conditions in the reflection mode. The temperature coefficient of resonant frequency was measured by inserting the cavity inside a thermal chamber and the shift in resonant frequency was measured from 25 to 80 °C.

Results and discussion

Pure samples of $\text{Ba}_8\text{CoTa}_6\text{O}_{24}$ and $\text{Ba}_8\text{NiTa}_6\text{O}_{24}$ end members were prepared first to confirm previous reports of their positive τ_f . Single phase samples were readily obtained after heating at 1475 °C. Their X-ray patterns could be completely indexed using a cell with the same 8-layer, $(cchc)_2$, hexagonal perovskite structure reported for the Zn and Ni analogs (Fig. 1) [2, 4, 6, 7].

The dielectric properties of dense samples of $\text{Ba}_8\text{CoTa}_6\text{O}_{24}$ and $\text{Ba}_8\text{NiTa}_6\text{O}_{24}$ were measured at low frequency and in the microwave region. The dielectric constants were similar to those reported previously: $\text{Ba}_8\text{CoTa}_6\text{O}_{24}$,

$\varepsilon_r = 29.7$; $\text{Ba}_8\text{NiTa}_6\text{O}_{24}$, $\varepsilon_r = 28.9$; however, the $Q \cdot f$ values, 39,700 at 8.8 GHz for Co and 50,900 at 8.9 GHz for Ni, were not as high as the values reported in Refs. [4, 5] (69,416 for Co and 81,758 for Ni). We also found small differences in the τ_f : $\text{Ba}_8\text{CoTa}_6\text{O}_{24}$, $+33.90$ ppm/°C for Co (compared to $+44$ in Ref. [4]) and $+22.2$ ppm/°C for Ni (compared to $+32$ in Ref. [4]). It is possible these differences are related to preferential orientation of the grains, which has been noted previously for these systems [6]. However, in agreement with the previous work τ_f for both compounds is opposite in sign to their corresponding cubic perovskites ($\text{Ba}(\text{Co}_{1/3}\text{Ta}_{2/3})\text{O}_3$, $\tau_f = -16$ ppm/°C; $\text{Ba}(\text{Ni}_{1/3}\text{Ta}_{2/3})\text{O}_3$, $\tau_f = -18$ ppm/°C) suggesting a zero τ_f microwave ceramic could exist in two-phase composites of either system [8, 9].

To confirm this hypothesis we explored the synthesis and properties of the Ni-based system: $(1-x)\text{Ba}(\text{Ni}_{1/3}\text{Ta}_{2/3})\text{O}_3 - (x)\text{Ba}(\text{Ni}_{1/8}\text{Ta}_{3/4})\text{O}_3$. X-ray patterns collected from samples with $x = 0.0, 0.05, 0.1, 0.2, 0.4, 0.5, 0.6, 0.8, 0.9$, and 1.0 are shown in Fig. 2. The patterns for $x = 0$ ($\text{Ba}(\text{Ni}_{1/3}\text{Ta}_{2/3})\text{O}_3$) and $x = 1.0$ ($\text{Ba}_8\text{NiTa}_6\text{O}_{24}$) were in agreement with those previously reported in the literature. No evidence was found for any significant solubility for either end-member and the X-ray patterns of the intermediate compositions could all be indexed in terms of a two-phase mixture of these phases. The stable two-phase

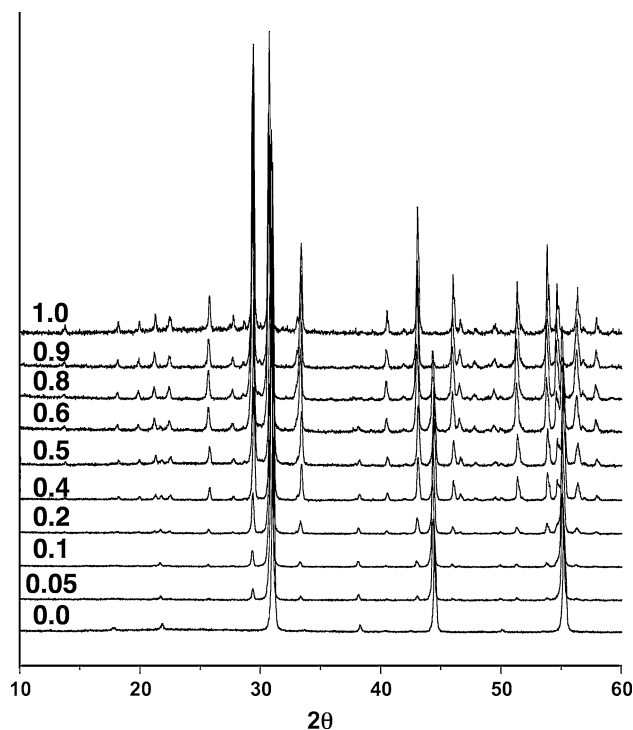


Fig. 2 Powder X-ray diffraction patterns of $(1-x)\text{Ba}(\text{Ni}_{1/3}\text{Ta}_{2/3})\text{O}_3 - (x)\text{Ba}(\text{Ni}_{1/8}\text{Ta}_{3/4})\text{O}_3$ for $x = 0, 0.05, 0.1, 0.2, 0.4, 0.5, 0.6, 0.8, 0.9, 1.0$

existence of the cubic and hexagonal perovskite phases formed the basis for the preparation of a family of thermodynamically compatible composite structures with a tuned dielectric response.

The lower sintering temperature of $\text{Ba}_8\text{NiTa}_6\text{O}_{24}$ (1400 °C) as compared to $\text{Ba}(\text{Ni}_{1/3}\text{Ta}_{2/3})\text{O}_3$ (~1610 °C) enhanced the densification of the two-phase $(1-x)\text{Ba}(\text{Ni}_{1/3}\text{Ta}_{2/3})\text{O}_3-(x)\text{Ba}(\text{Ni}_{1/8}\text{Ta}_{3/4})\text{O}_3$ samples which could be sintered to >95% theoretical density at 1500 °C [9]. An SEM micrograph of the polished and thermally etched surface of a pellet with $x = 0.4$ (Fig. 3) reveals the microstructure exhibits minimal porosity and is comprised of larger grains of $\text{Ba}_8\text{NiTa}_6\text{O}_{24}$ (4–8 μm) and smaller grained $\text{Ba}(\text{Ni}_{1/3}\text{Ta}_{2/3})\text{O}_3$ (1–2 μm). The dielectric properties of the as-sintered $(1-x)\text{Ba}(\text{Ni}_{1/3}\text{Ta}_{2/3})\text{O}_3-(x)\text{Ba}(\text{Ni}_{1/8}\text{Ta}_{3/4})\text{O}_3$ ($0 \leq x \leq 1$) ceramics are listed in Table 1. The two-phase composites show an essentially linear variation of the dielectric constant across the system.

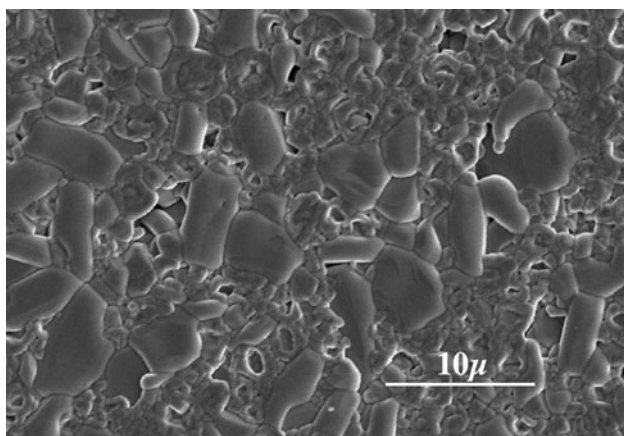


Fig. 3 SEM micrograph of $0.6\text{Ba}(\text{Ni}_{1/3}\text{Ta}_{2/3})\text{O}_3-0.4\text{Ba}(\text{Ni}_{1/8}\text{Ta}_{3/4})\text{O}_3$ after sintering at 1500 °C

Table 1 Microwave dielectric properties of $(1-x)\text{Ba}(\text{Ni}_{1/3}\text{Ta}_{2/3})\text{O}_3-(x)\text{Ba}(\text{Ni}_{1/8}\text{Ta}_{3/4})\text{O}_3$ composites

x	After sintering		After annealing (1400 °C for 48 h)		τ_f (ppm/°C)
	ϵ	$Q \cdot f$	ϵ	$Q \cdot f$	
0.05	23.2	41500 (9.7 GHz)	23.02	66349 (9.6 GHz)	-20.8
0.1	24.0	43340 (9.4 GHz)	23.68	50414 (9.8 GHz)	-10.7
0.2	23.7	38680 (9.7 GHz)	22.16	32623 (10.1 GHz)	-10.3
0.4	24.6	47750 (9.3 GHz)	24.99	61890 (9.3 GHz)	-0.4
0.5	25.1	47470 (9.4 GHz)	25.65	66682 (9.4 GHz)	+3.2
0.6	26.4	41130 (8.9 GHz)	26.25	54189 (9.03 GHz)	+7.8
0.8	28.2	61750 (8.9 GHz)	27.82	65286 (9.03 GHz)	+22.3
0.9	28.0	54220 (8.7 GHz)	27.65	68683 (8.9 GHz)	+23.0
1.0	28.9	50870 (9.0 GHz)	28.59	63000 (9.0 GHz) ^a	+22.2

^a Annealed at 1325 for 48 h

The $Q \cdot f$ increases with x , though the variation is not monotonic; the highest value (62,000) was recorded for $x = 0.8$.

The dielectric loss of the $\text{A}(\text{B}_{1/3}^{\text{I}}\text{B}_{2/3}^{\text{II}})\text{O}_3$ family of microwave perovskites is well known to respond to slow cooling or post-sintering lower temperature annealing [10]. These changes are associated with alterations in the ordering of the cations on the B-site sub-lattice through enhanced positional order and/or increases in the size of the different orientational domains of their 1:2 ordered structure [10–12]. Therefore, the sintered pellets were annealed for 48 h at 1400 °C and their structure and dielectric properties were re-examined. While the lower temperature treatment had no significant effect on the dielectric constant the $Q \cdot f$ values increased significantly, particularly for the $\text{Ba}(\text{Ni}_{1/3}\text{Ta}_{2/3})\text{O}_3$ -rich compositions, see Table 1. To ascertain the effect of the annealing on the chemical ordering in the $\text{Ba}(\text{Ni}_{1/3}\text{Ta}_{2/3})\text{O}_3$ component, X-ray diffraction patterns were collected from the top and bottom surface of the pellets before and after annealing. Figure 4 shows the X-ray data collected from a sample with $x = 0.05$. The width of the superstructure peaks from the chemical ordering show a clear decrease after the heat treatment and the integrated intensity of the ordering reflections show a small increase. The increase in $Q \cdot f$ for these samples is therefore consistent with the previous observations of improvements in Q with enhanced chemical order.

After the lower temperature annealing the samples with higher x values, i.e., $\text{Ba}_8\text{NiTa}_6\text{O}_{24}$ -rich composites, also show improvements in their $Q \cdot f$ (Table 1). Although part of the enhanced $Q \cdot f$ could be associated with increased cation order in the minority $\text{Ba}(\text{Ni}_{1/3}\text{Ta}_{2/3})\text{O}_3$ phase, the

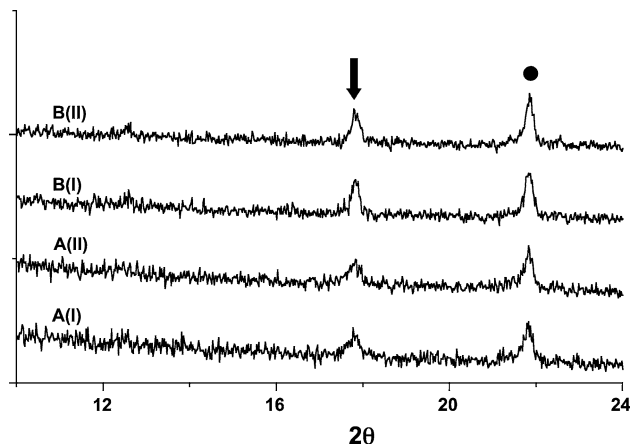


Fig. 4 Low angle region of the X-ray diffraction patterns of the top (I) and bottom (II) surfaces of $(0.95)\text{Ba}(\text{Ni}_{1/3}\text{Ta}_{2/3})\text{O}_3-(0.05)\text{Ba}(\text{Ni}_{1/8}\text{Ta}_{3/4})\text{O}_3$ pellets: (A) after sintering; (B) after annealing at 1400 for 48 h. Arrow highlight the (100) superstructure reflection, circle represents the fundamental reflection

improvement for these samples and pure $\text{Ba}_8\text{NiTa}_6\text{O}_{24}$ indicates other factors must also be involved. We investigated the effect of annealing on the microstructure of $\text{Ba}_8\text{NiTa}_6\text{O}_{24}$ by comparing the microstructure of the as-sintered samples to those annealed for extended periods at lower temperature (in this case 1325 °C). As shown in Fig. 5 the extended annealing induces significant grain growth with the length and width of the “bar-shaped” grains increasing from $\sim 10 \times 2$ to $>100 \times 20$ μm . Consistent with previous studies, it is also evident the grains of $\text{Ba}_8\text{NiTa}_6\text{O}_{24}$ show considerable preferential orientation [6]. We believe these factors combined are responsible for the small improvements in $Q \cdot f$ observed after annealing composites where $\text{Ba}_8\text{NiTa}_6\text{O}_{24}$ is the majority phase.

The variation of τ_f in the two-phase composites, Table 1, is an essentially linear function of composition. As conjectured, given the opposite sign of τ_f for the two end members the temperature coefficient can be tuned to a

zero value. Our experiments indicate the zero value occurs at a composition with $x = 0.4$. This zero τ_f ceramic has $\varepsilon = 24.6$ and $Q \cdot f = 47,700$.

It is likely the utility of these perovskites in permitting the design of high Q , zero τ_f cubic/hexagonal composites could be extended to other tantalate and niobate based systems. In particular the Co tantalate system, where the end members also have opposite signs of τ_f , would be a logical candidate for study.

Conclusions

Compositions lying between $\text{Ba}(\text{Ni}_{1/3}\text{Ta}_{2/3})\text{O}_3$ and $\text{Ba}_8\text{NiTa}_6\text{O}_{24}$ ($=\text{Ba}(\text{Ni}_{1/8}\text{Ta}_{3/4})\text{O}_3$) were prepared and investigated. X-ray diffraction revealed these samples form stable two-phase mixtures of the respective cubic and hexagonal end members. Measurement of the dielectric properties at microwave frequencies demonstrated the temperature coefficient of the resonant frequency of the two-phase composites could be tuned to a zero value. The zero τ_f ceramic has $\varepsilon = 24.6$ and a high $Q \cdot f = 47,700$. The quality factors could be improved through a post-sintering annealing treatment that enhances the ordering of the cubic perovskite component and increases the grain size of the hexagonal end-member.

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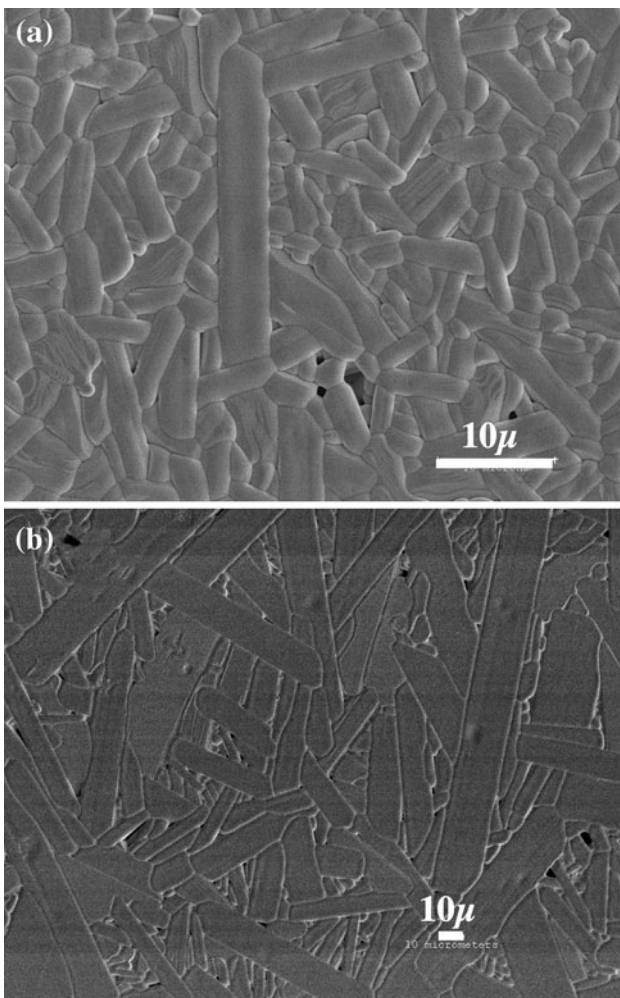


Fig. 5 SEM micrograph of $\text{Ba}_8\text{NiTa}_6\text{O}_{24}$: **a** after sintering; **b** after a subsequent anneal at 1325 °C for 48 h